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(54)   Blade root and rotor disc groove contour

(57)   An improved connection of blades (12) on a rotor disc (22) of a gas turbine, of the type in which a root (10) of each blade (12) is inserted in a seat (20) of the disc (22) which is complementary to the blade, wherein the root (10) is in the shape of an overturned isosceles triangle, with the two sides which converge at the base each having a grooved profile such as to form a series of teeth (14) and with a lower end (16) of the root (10) which is formed by the joined connection of the two lower teeth (14) of the two sides of the root (10), the teeth (14) of the root (10) corresponding to grooves (24) in the seat (20) and the lower end (16) of the root (10) corresponding to an end groove (26) in the seat (20). This series of grooves (24) extends along a line which is inclined relative to the axis of the seat (20) by an angle β_1 of between 17° and 23°, and the grooves (24) have straight sides with inclinations relative to the axis of the seat (20) of angles α_1 and α_2, wherein α_1 is between 42° and 48° whereas α_2 is between 94° and 100°.

Fig.1
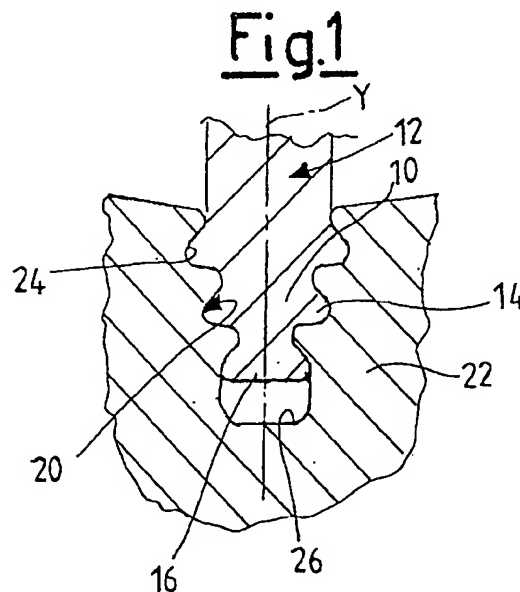
Description

[0001]   The present invention relates to an improved connection of blades on a rotor disc of a gas turbine.

[0002]   As is known, gas turbines are machines which consist of a compressor and a turbine with one or more stages, wherein these components are connected to each other by a rotary shaft and wherein a combustion chamber is provided between the compressor and the turbine. The gas output from the combustion chamber, which has a high temperature and a high pressure, reaches through corresponding pipes the different stages of the turbine, which transforms the enthalpy of the gas into mechanical energy available to a user.

[0003]   In turbines with two stages the gas is processed in the first stage of the turbine in temperature and pressure conditions which are very high and undergoes a first expansion there. Then, in the second stage of the turbine it undergoes a second expansion in temperature and pressure conditions which are lower than those used in the preceding stage.

[0004]   It is also known that in order to obtain the maximum performance from a specific gas turbine it is necessary for the temperature of the gas to be as high as possible. However, the maximum temperature values which can be obtained in use of the turbine are limited by the resistance of the materials which are used at present.

[0005]   It is also known that in gas turbines the rotor blades do not form a single body with the rotor disc, but are retained by means of their base extensions in appropriate seats provided on the circumference of the disc. In particular, the seats used at present have sides with a grooved profile, in which the end portion of the foot or root of the corresponding blade is engaged.

[0006]   A problem which is particularly significant in the present art is therefore that of guaranteeing an optimal connection of the blades on the rotor disc, in all the conditions of functioning of the machine. It should be noted that the method of connection of the blades on the rotor disc represents a crucial aspect of the design of any rotor, taking into account the fact that the disc must withstand satisfactorily and reliably the loads generated by the blades without giving rise to breakages or other similar problems. It is also known that during functioning of the machine, the rotor blades are subjected to high stresses both in the radial direction, and to a lesser extent in the axial direction. The radial stresses are caused by the high speed of rotation of the turbine, whereas the axial stresses are caused by the effect produced by the flow of gas on the profiled surfaces of the blades. The same flow of gas transmits to the blades the circumferential component of the stress which makes it possible to gather useful power at the drive shaft.

[0007]   However, the method of connection of the blades must use the smallest possible dimensions, occupying truly limited spaces, such as to reduce the as-sembly constituted by the rotor disc and blades to the smallest possible dimensions. Furthermore, nowadays, the trend is to obtain gas turbines with increasingly high performance levels. This involves having to increase both the speed of rotation and the combustion temperature. There is consequently also an increase in the temperature of the gases which expand in the stages of the turbine against the blades.

[0008]   This gives rise to an increase in the stresses on the connection between the blades and rotor discs of the turbine, with increasingly great difficulty in guaranteeing an adequate service life of the blades and rotor discs.

[0009]   At present the connection most widely used is that which is commonly known as the "pine tree" type. It consists of shaping the root or foot of the blade such that its cross-section assumes a characteristic shape which is reminiscent of an overturned pine tree. In this particular form the sides of the root have a grooved profile such as to form a series of teeth with a rounded profile; otherwise, in its lower end the root is formed by the connection of the two lower teeth of the two sides. These roots are connected to seats or coupling slots complementary to them which are provided on the circumference of the rotor disc, such that grooves in the sides of the seat correspond to the teeth of the root and a groove at the base of the seat corresponds to the lower end of the root. In conventional embodiments, these seats for the roots of the blades extend in a direction which is substantially parallel to the axis of the rotor disc.

[0010]   On the other hand in different embodiments, the seats for the roots extend substantially in a direction which is inclined relative to the axis of the disc itself.

[0011]   This type of connection has areas of particular concentration of stress which can be determined more specifically as being at the bottom of the groove, on the base of the seat, and on the base of the grooves of each tooth, which constitutes the actual connection profile.

[0012]   The main object of the present invention is thus to eliminate the above-described disadvantages and in particular to provide an improved connection for blades on a rotor disc of a gas turbine which makes it possible to reduce the concentrations of stress, thus making it possible to increase the speed of rotation of the machines or to increase the temperature of the fluid, or an appropriate combination of these factors.

[0013]   Another object of the present invention is to provide an improved connection of blades on a rotor disc of a gas turbine, which permits easy assembly and dismantling, according to requirements, of the blades of the different stages of the turbine.

[0014]   Another object of the present invention is to provide an improved connection of blades on a rotor disc of a gas turbine which is also highly reliable.

[0015]   A further object of the present invention is to obtain a service life of the components which is far longer than that which can be obtained at present with the connections used.

[0016] A further object of the present invention is to provide an improved connection of blades on a rotor disc of a gas turbine which is particularly simple and functional, has relatively low costs, and can be produced by means of conventional processing.

[0017] These objects and others according to the present invention are achieved by providing an improved connection of blades on a rotor disc of a gas turbine as described in claim 1.

[0018] Further characteristics are indicated in the subsequent claims.

[0019] According to the invention it has also been possible to determine that the reduction of the maximum values of the stresses in the areas of concentration of the forces gives rise to a considerable increase in the life of the components.

[0020] The characteristics and advantages of an improved connection of blades on a rotor disc of a gas turbine according to the present invention will become more apparent from the following description provided by way of non-limiting example with reference to the attached schematic drawings, in which:

Figure 1 is a cross-section which shows a connection between a root of a blade and a seat or end slot of a rotor disc of the "pine tree" type according to the known art;

Figure 2 is a cross-section which shows the partial profile of a root of a blade, produced according to the description of the present invention; and

Figure 3 is a cross-section which shows the partial profile of a seat or end slot of a rotor disc, in which the root of the blade in figure 2 is inserted.

[0021] Figure 1 shows a connection according to the known art, between a root or foot 10 of a blade 12 and a seat or end slot 20 of a rotor disc 22 of a gas turbine. The root or foot 10 of the blade 12 has a characteristic shape, substantially of an overturned isosceles triangle, with the two sides which converge at the base. This shape is symmetrical relative to the axis Y of the root 10. The two sides or flanks have a grooved profile such as to form a series of teeth 14 with a rounded profile. In the example shown in figure 1, three teeth 14 are provided for each side of the root 10.

[0022] A lower end 16 of the root 10 is formed by the connection of the two lower teeth 14 of the two sides of the root 10 itself. These roots 10 are connected to the seats or coupling slots 20 complementary to them which are provided on a circumference of the rotor disc 22, such that grooves 24 on the sides of the seat 20 correspond to the teeth 14 of the root 10, and an inner end groove 26 at the base of the seat 20 corresponds to the lower end 16 of the root 10.

[0023] Figures 2 and 3 show respectively partial profiles of the root 10 and of the seat 20 complementary to it, of a connection according to the present invention. In the example shown the root 10 has four teeth 14 for each side. A further tooth 14 which is present at a lower end of the side of the root 10 is connected by means of a connection to the similar tooth 14 which is present on the other side in order to form the lower end 16 of the root 10. Correspondingly the seat 20 has four grooves 24 for each side. A further groove 24 which is present at a lower end of the side of the seat 20 is connected by means of a connection to the similar groove 24 which is present on the other side in order to form the inner end groove 26 of the seat 20.

[0024] Figure 3 shows the geometric variables which characterise the profile of the seat 20, and consequently also the root 10, which is complementary to the seat 20 itself. The series of grooves 24 extends along a line X which is inclined relative to the axis Y of the seat 20 by an angle β_1. Consequently the side of the seat 20 also extends according to this inclination.

[0025] The four grooves 24 have straight sides with inclinations of angles α_1 and α_2 relative to the axis Y of the seat 20, wherein α_1 is the angle of the side facing the exterior of the rotor disc 22. The two sides of the groove 24 thus form a groove angle α_g which is equal to α_2 subtracted from α_1. The groove 24 is connected at its base according to an arc of a circumference with a radius R_4. In addition, between the four grooves 24 and between the lower groove 24 and the inner end groove 26, there are four connections according to an arc of a circumference with a radius R_4.

[0026] The side with the angle α_1 of the upper groove 24 is connected towards the exterior of the rotor disc 22 according to an arc of a circumference with a radius R_3.

[0027] The inner end groove 26 is in the shape of an overturned omega, with the two symmetrical upper sides disposed according to angles α_1 relative to the axis Y of the seat 20. These sides are connected to one another according to four arcs of four circumferences which are symmetrical relative to one another, in pairs. More specifically, their upper side is connected initially according to an arc of a circumference with a radius R_1 and a centre determined by a height H_1 relative to the base of the inner end groove 26 and by a distance D_1 relative to the axis Y of the seat 20.

[0028] This arc of a circumference is followed by an arc of a circumference with a radius R_2 and a centre determined by a height H_2 relative to the base of the inner end groove 26 and by a distance D_2 relative to the axis Y of the seat 20.

[0029] Complementarily, as can be seen in figure 2, the tooth 14 of the root 10 also has straight sides with inclinations relative to the axis Y of the root 10 with the same angles α_1 and α_2, wherein α_1 is the angle of the side which faces the blade 12. The two sides of the tooth 14 thus form a toothing angle α_d which is equal to α_2 subtracted from α_1, and is thus equal to the groove angle α_g. The tooth 14 is connected according to an arc of a circumference with a radius R_4. In addition, between the

four teeth 14 and between the lower tooth 14 and the lower end 16 of the root, there exist four connections according to an arc of a circumference with a radius R_4.

[0030] The side with the angle α_1 of the upper tooth 14 is connected to the blade 12 according to an arc of a circumference with a radius R_3.

[0031] The lower end 16 is in the shape of an over-turned omega, with the two symmetrical upper sides disposed according to second angles α_1 relative to the axis Y of the root 10. These sides are connected to one another according to four arcs of four circumferences which are symmetrical relative to one another, in pairs. More specifically, their upper side is connected initially according to an arc of a circumference with a radius R_1 and a centre determined by a height H_1 relative to the lower end 16 of the root 10 and by a distance D_1 relative to the axis Y of the root 10 itself.

[0032] This arc of a circumference is followed by an arc of a circumference with a radius R_2 and a centre determined by a height H_2 relative to the lower end 16 of the root 10 and by a distance D_2 relative to the axis Y of the root 10 itself.

[0033] To summarise, the eight teeth 14 of the two sides of the root 10 and the lower end 16 of the root 10 itself are inserted respectively in the eight grooves 24 in the two sides of the seat 20 and the inner end groove 26 of the seat 20 itself.

[0034] In addition, the two connections with a radius R_3 of the root 10 and of the seat 20 are also made to fit together simultaneously with the insertion of the root 10 in the seat 20, which is carried out by making the root 10 slide along an axial direction into the corresponding seat 20.

[0035] By means of its application with analysis of the stresses, the present invention has made it possible to reduce the concentrations of stress and to indicate a suitable geometry for the profiles of contact between the roots 10 of the blades 12 and seats 20 of the rotor disc 22.

[0036] The ratios between the radii R_1, R_2, R_3 and R_4, the heights H_1 and H_2, the distances D_1 and D_2 and the angles α_1, α_2 and β_1 must be considered fundamental. In fact these ratios determine the form of the teeth 14, as well as of the lower end 16 of the root 10, which lead to the improved connection according to the present invention. Taking as a reference the radius R_4, it has been determined according to the present invention that the connection is optimised if the following ratios exist:

the ratio between R_3 and R_4 is between 1.8 and 2.2, including extreme values;

the ratio between R_1 and R_4 is between 1.8 and 2.2, including extreme values;

the ratio between R_2 and R_4 is between 5.5 and 6, including extreme values.

[0037] Simultaneously, the following ratios must exist for the angles:

the angle α_1 is between 42° and 48°, including extreme values;

the angle α_2 is between 94° and 100°, including extreme values;

the angle β_1 is between 17° and 23°, including extreme values.

[0038] With these ratios, the groove angle α_g, which is equal to the toothing angle α_d is between 46° and 58°, including extreme values.

[0039] The heights H_1 and H_2 and the distances D_1 and D_2 are determined as a direct consequence of the general dimensions of the root 10, i.e. substantially after having determined the height of the root 10.

[0040] According to the present invention it is thus found that the best results are obtained by using roots 10 with four teeth 14, according to the embodiment shown in figures 2 and 3, or roots 10 with five teeth 14.

[0041] The description provided makes apparent the characteristics of the improved connection according to the present invention for blades on a rotor disc of a gas turbine, as well as its advantages, which it should be noted include:

- increase in the service life of the components;

- increase in the speed of rotation of the machines, or increase in the temperature of the fluid, or an appropriate combination of the two aspects; and

- costs which are low compared with the known art, since the profiles can always be obtained by broaching, as is already the case for the connections according to the known art.

Claims

1. Connection of blades (12) on a rotor disc (22) of a gas turbine, of the type in which a root or foot (10) of each blade (12) is inserted in a seat or end slot (20) of the disc (22) which is complementary to the blade, wherein the said root (10) is in the shape of an overturned isosceles triangle, with the two sides which converge at the base each having a grooved profile such as to form a series of teeth (14) and with a lower end (16) of the root (10) which is formed by the joined connection of the two lower teeth (14) of the two sides of the root (10), the said teeth (14) of the root (10) corresponding to grooves (24) provided in the sides of the seat (20) and the said lower end (16) of the root (10) corresponding to an inner end groove (26) provided in the base of the seat

(20), **characterised in that** the series of the said grooves (24) extends along a line (X) which is inclined relative to the axis (Y) of the seat (20) by an angle β_1 of between 17° and 23°, including extreme values, and **in that** the said grooves (24) have straight sides with inclinations relative to the axis (Y) of the seat (20) of angles α_1 and α_2, wherein α_1 is the angle of the side which faces the exterior of the rotor disc (22) and is between 42° and 48°, including extreme values, whereas α_2 is between 94° and 100°, including extreme values.

2. Connection according to claim 1, **characterised in that** the said grooves (24) are connected on the base according to an arc of a circumference with a radius R_4, connections being provided between the said grooves (24) according to an arc of a circumference which also has a radius R_4, **in that** the side with the angle α_1 of the upper groove (24) is connected towards the exterior of the rotor disc (22) according to an arc of a circumference with a radius R_3, and **in that** the inner end groove (26) is in the shape of an overturned omega, with the two symmetrical upper sides disposed according to second angles α_1 relative to the axis of the seat (20), and are connected to one another according to four arcs of a circumference which are symmetrical relative to one another, in pairs, and specifically according initially to arcs of a circumference with a radius R_1 and subsequently arcs of a circumference with a radius R_2, wherein the radii R_1, R_2 and R_3 have the following ratios to the radius R_4:

$$1.8 \leq R_3/R_4 \leq 2.2;$$

$$1.8 \leq R_1/R_4 \leq 2.2;$$

$$5.5 \leq R_2/R_4 \leq 6.$$

3. Connection according to claim 1, **characterised in that** the said connection according to an arc of a circumference with a radius R_1 is produced using as the centre the point determined by a height H_1 relative to the base of the inner end groove (26) and by a distance D_1 relative to the axis of the seat (20), and **in that** the said connection according to an arc of a circumference with a radius R_2 is produced using as the centre the point determined by a height H_2 relative to the base of the inner end groove (26) and by a distance D_2 relative to the axis of the seat (20), wherein the said centres are consequently determined on the basis of the general dimensions of the depth of the seat (20).

4. Connection according to claim 1, **characterised in**

that an angle with a groove α_g, which is equal to the angle α_2 subtracted from the angle α_1, is between 46° and 58°, including extreme values.

5. Connection according to claim 1, **characterised in that** the said seat (20) has eight grooves (24) which are symmetrical in pairs, and an inner end groove (26).

6. Connection according to claim 1, **characterised in that** the said seat (20) has ten grooves (24) which are symmetrical in pairs, and an inner end groove (26).
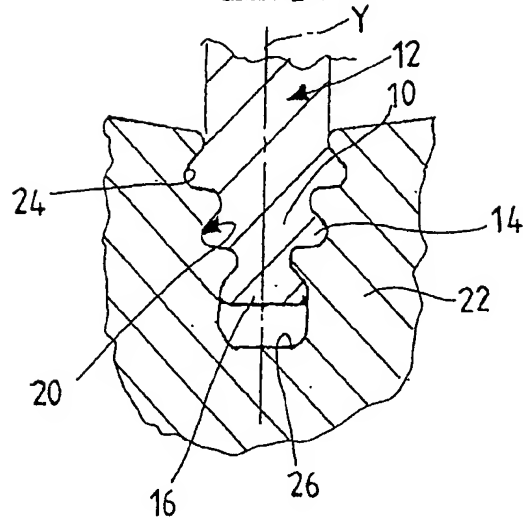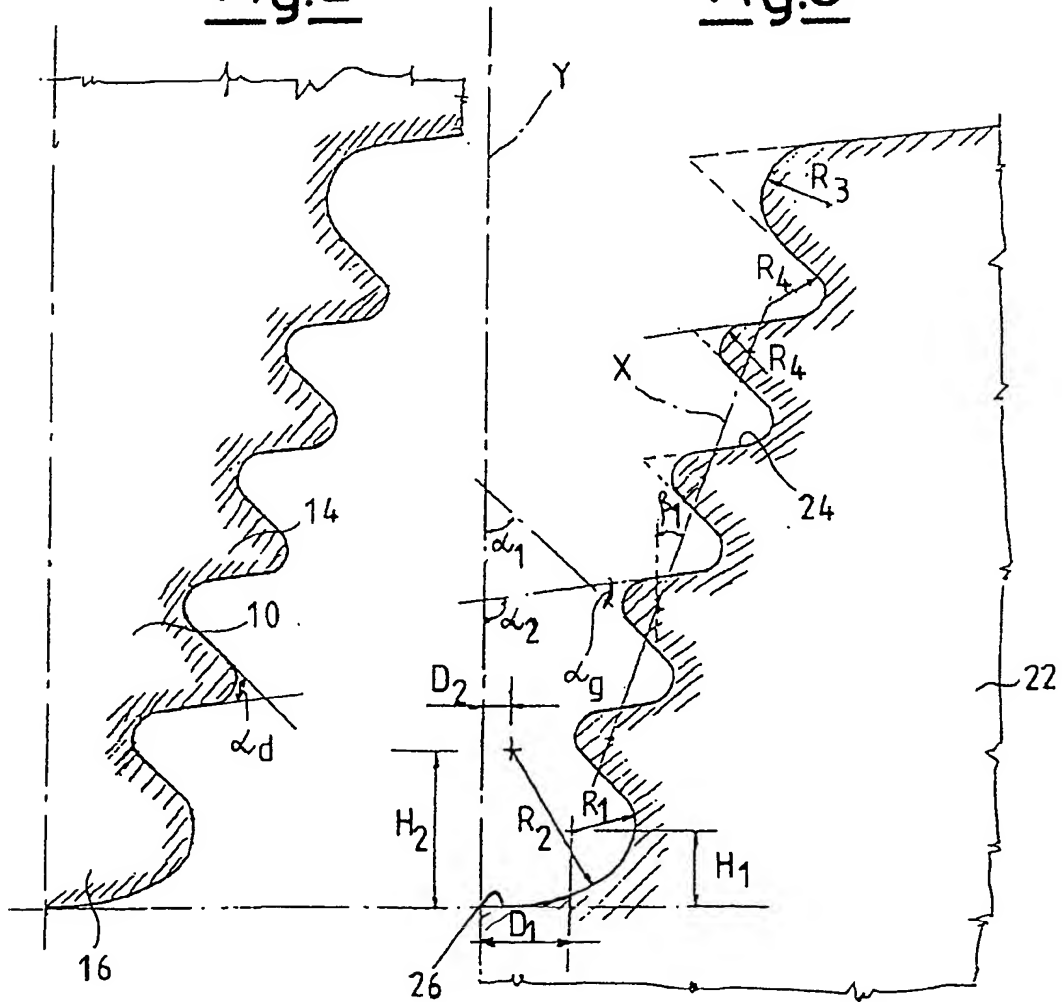
Fig.1

Fig.2

Fig.3